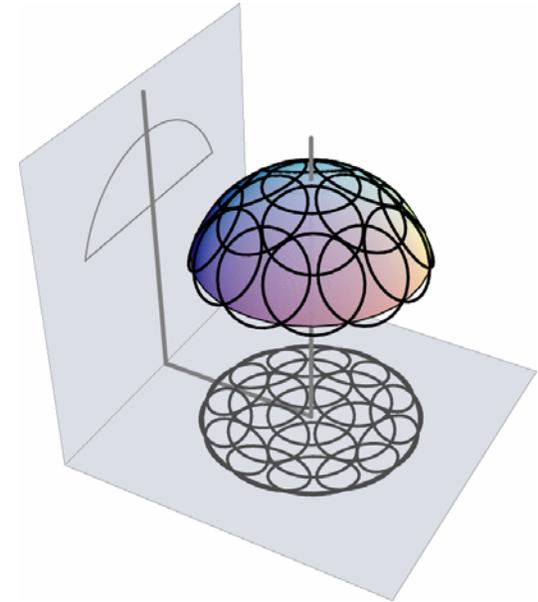
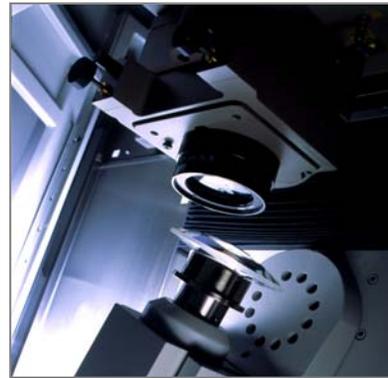


Subaperture stitching interferometer (SSI)



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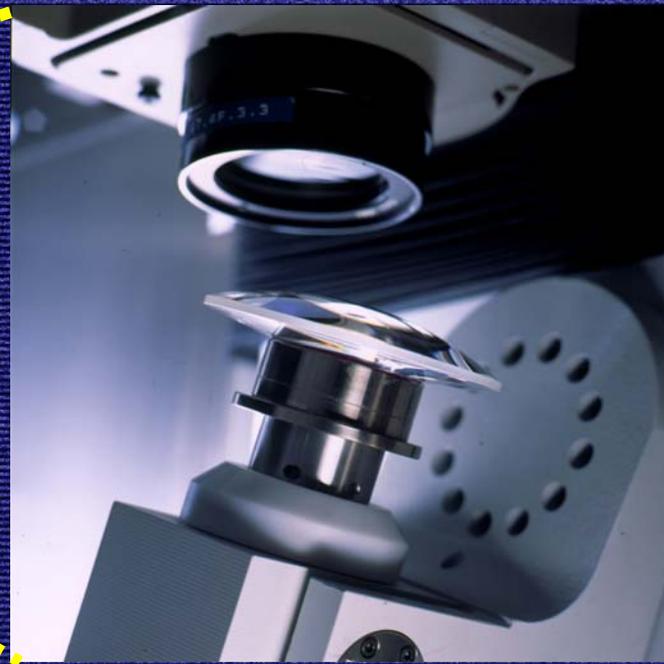
[Acknowledgements:](#)

Dr. Jim Kirsch

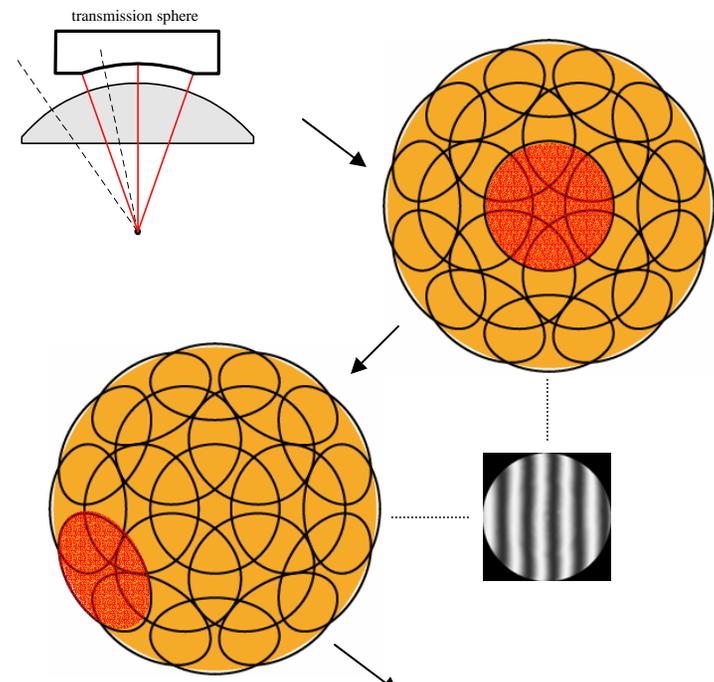
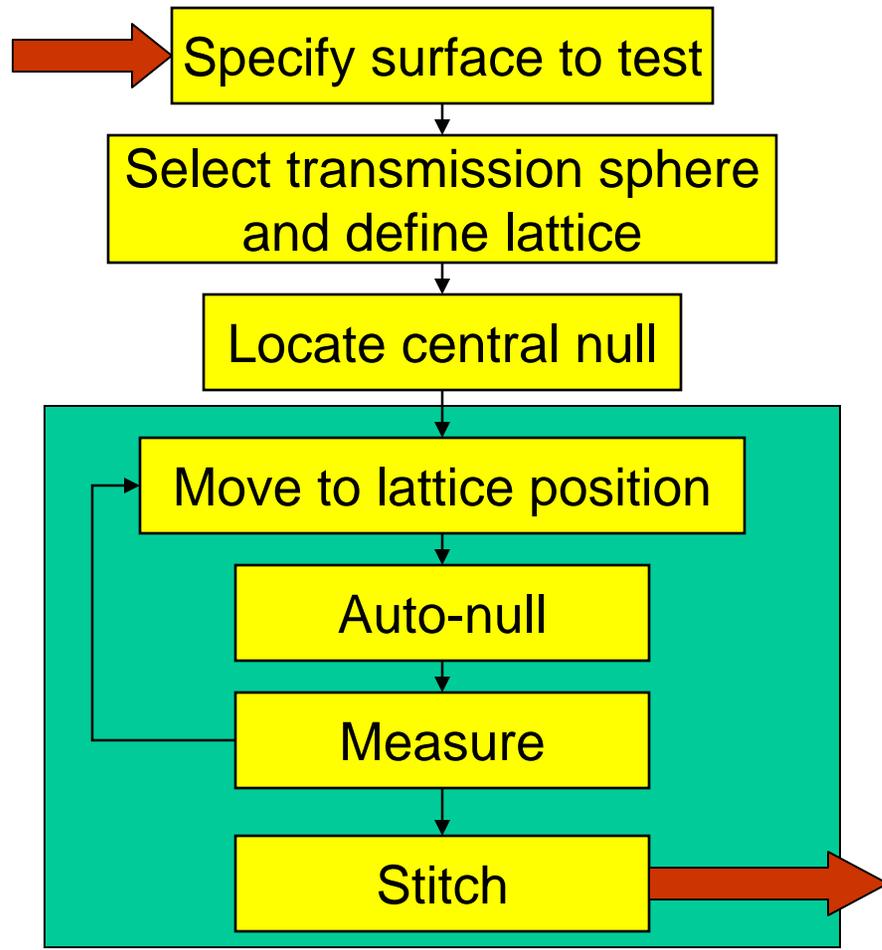
U.S. Army RDECOM

What is QED's Subaperture Stitching Interferometer?

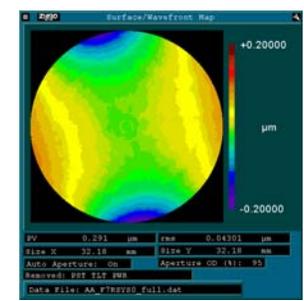
- ❖ Precision six axis machine
 - ❖ **Engineered in cooperation with Schneider Opticmachines**
- ❖ Standard Zygo 4" or 6" interferometer
- ❖ QED control software
 - ❖ **Measurement process automation + advanced algorithms**



SSI measurement process



Full-aperture map



Overview of stitching benefits

❖ Increase lateral dynamic range

- ❖ Increased lateral range by a factor of XF (“Extension Factor”)
 - ❖ Includes large numerical apertures (domes, hemispheres, etc.)
- ❖ Can improve lateral resolution (data density)

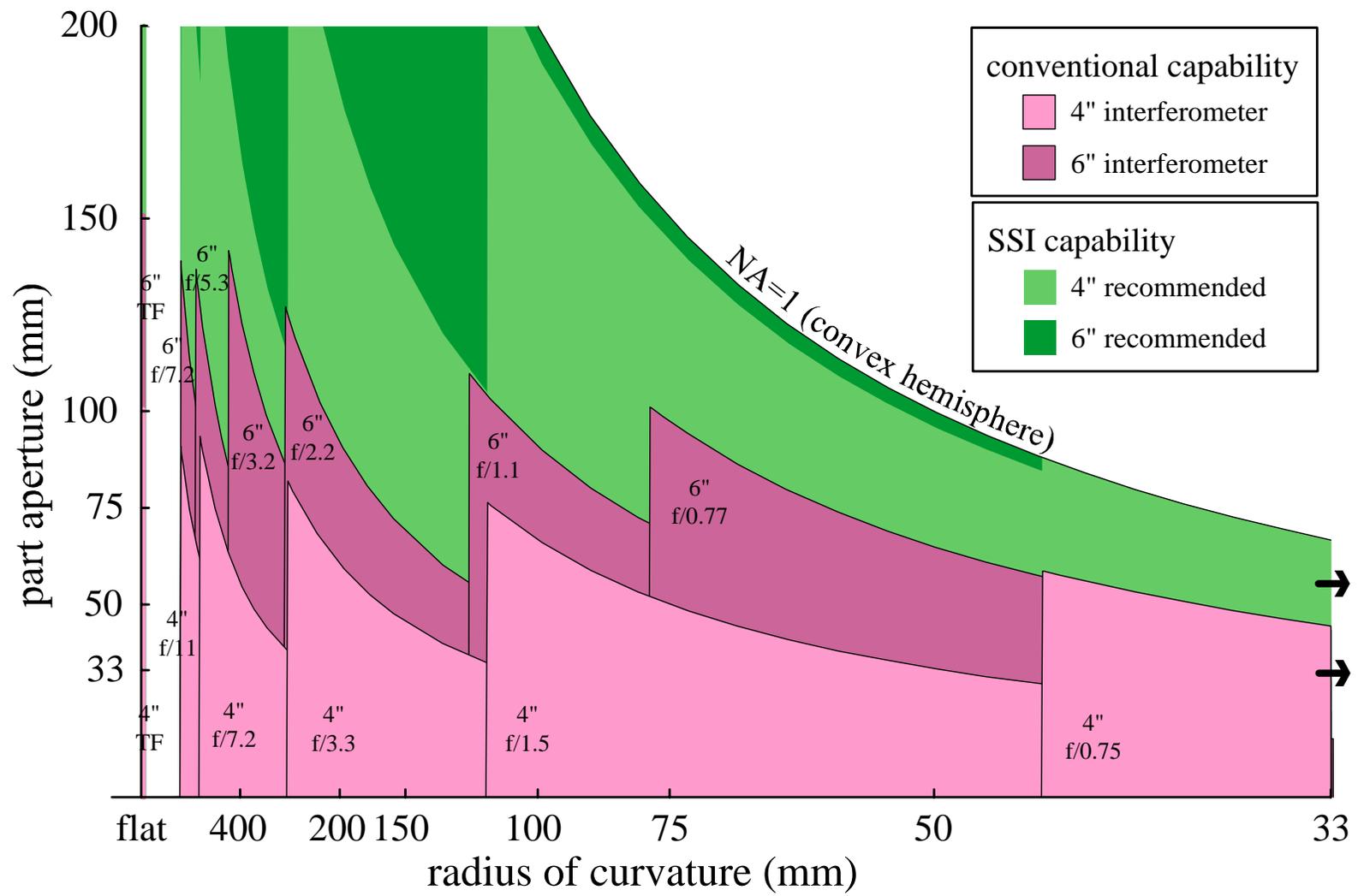
❖ Superior accuracy

- ❖ Automatic computation or measurement of reference wave
- ❖ Calculation of mapping errors (pixel scale, distortion)

❖ Increased longitudinal range

- ❖ Asphericity is “spread” among the subapertures, gain $\sim XF^2$
 - ❖ One factor of XF from magnification
 - ❖ Another factor $\sim XF$ from fitting a local best-fit sphere
 - ❖ *Demonstrate this effect on later slides*

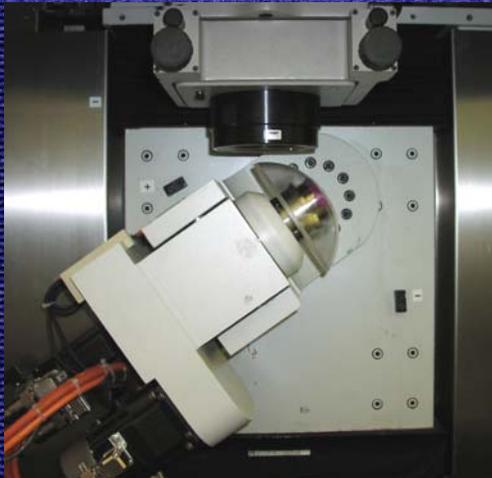
Extended lateral range



Sample of parts that can be measured on the current SSI

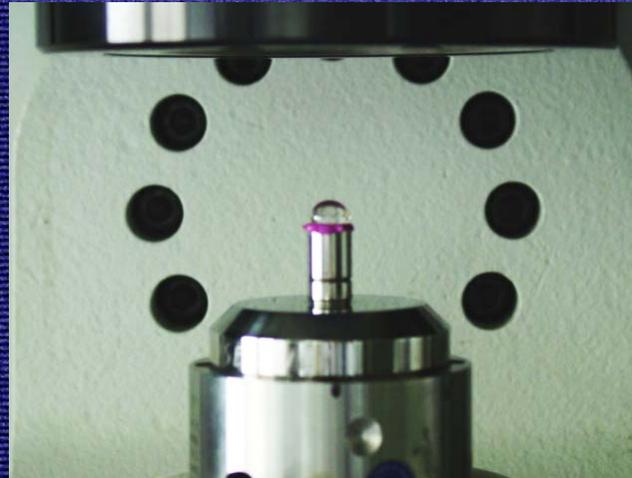
- ❖ Measures surfaces that have traditionally challenged commercial interferometers
 - ❖ Aperture up to 200 mm, angle up to 90° (hemisphere)

Large dome



Ø: 148 mm
R: 82 mm
NA: 0.90 (64°)

Small hemisphere



Ø: 9 mm
R: 4.5 mm
NA: 1.0 (90°)

Large convex



Ø: 200 mm
R: 500 mm
NA: 0.2 (12°)

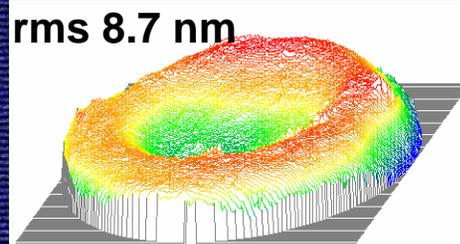
Stitch / full aperture cross-test

❖ Concave: aperture 80, radius 126 mm

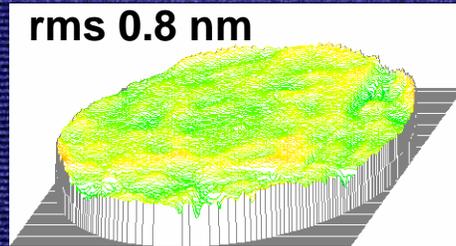


Two-sphere

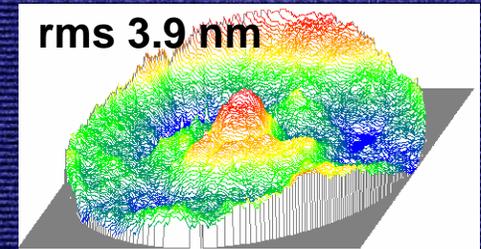
**Test surface
(scale 50 nm)**



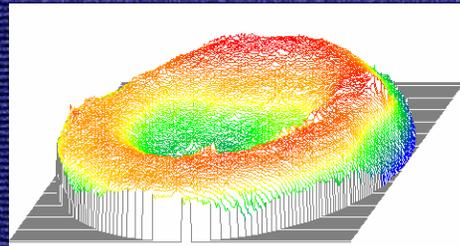
**Difference from
two-sphere test
surface
(scale 20 nm)**



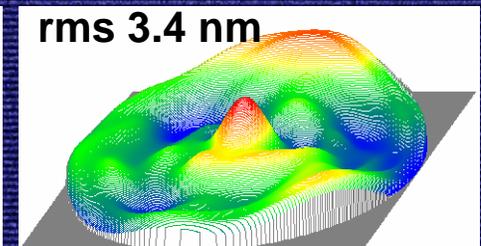
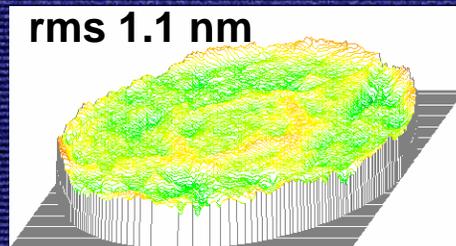
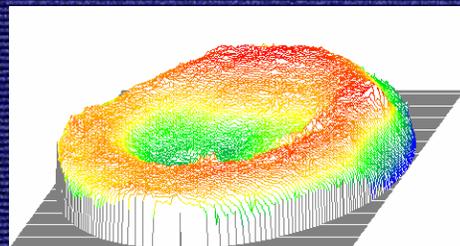
**Reference surface
(scale 20 nm)**



**Stitched
(reference:
two-sphere)**



**Stitched
(reference:
calculated, 230
Zernike terms)**



Transmission sphere cross-test

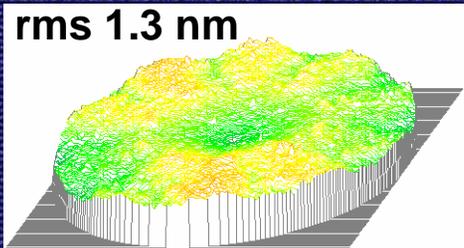
- ❖ Convex: aperture 80, radius 126 mm



- ❖ Not testable with 4" f/1.5 or 6" f/1.1
- ❖ Stitch with 4" f/3.3 and 4" f/7.2

Difference between f/3.3 and f/7.2 stitches

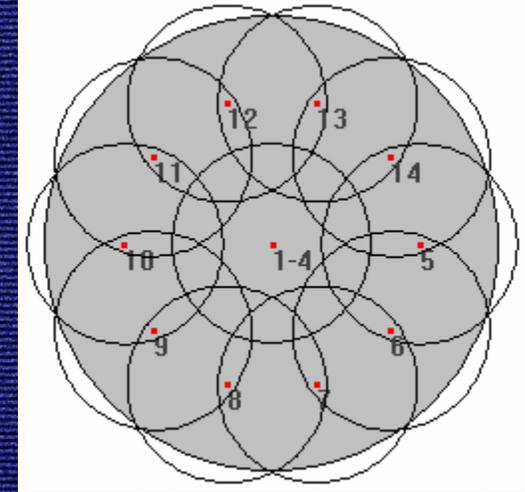
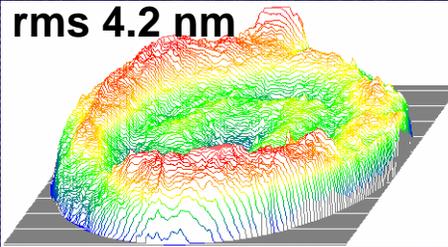
rms 1.3 nm



Still quite accurate, even with many subapertures

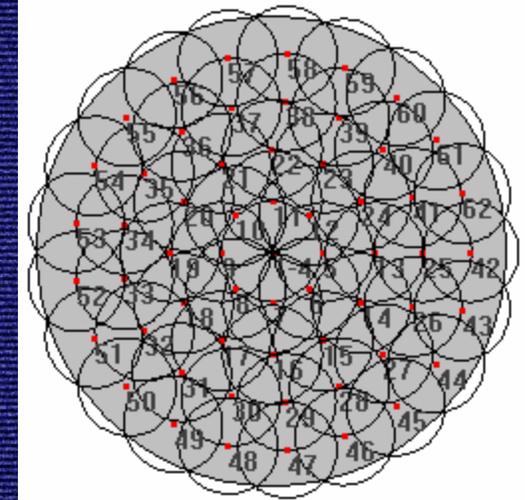
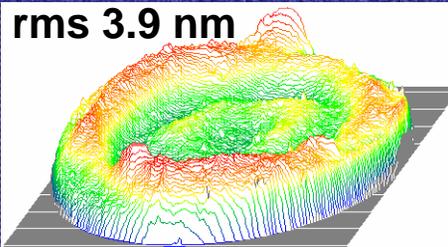
f/3.3
(36 mm field of view)
14 subapertures
XF = 2.2

rms 4.2 nm



f/7.2
(17 mm field of view)
62 subapertures
XF = 4.7

rms 3.9 nm

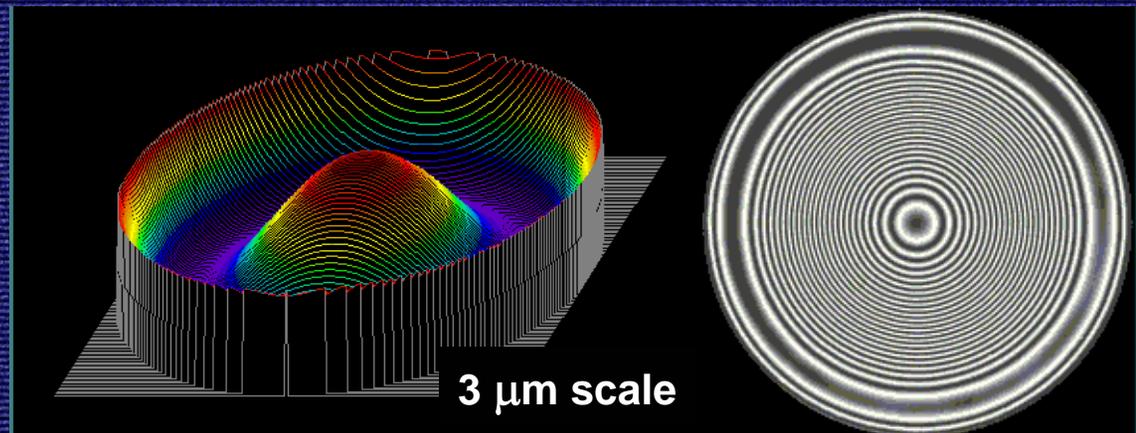


Non-null test example

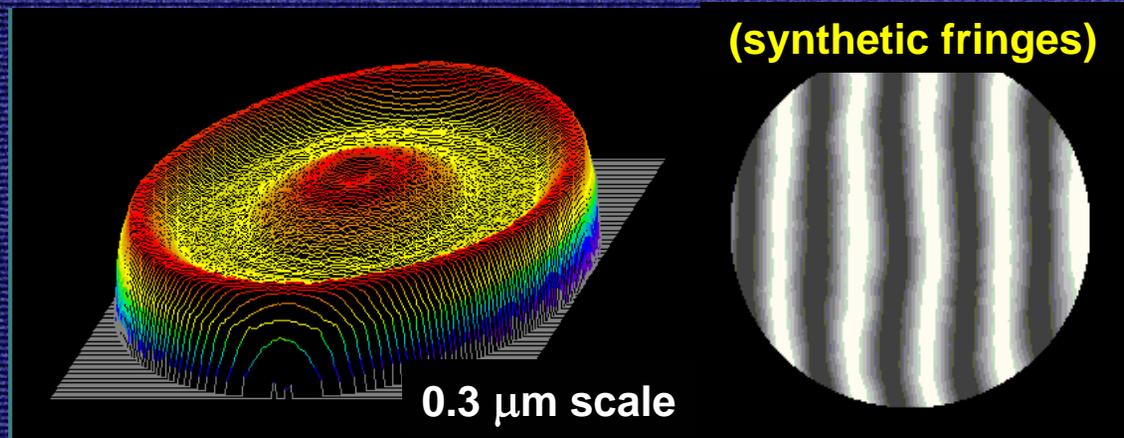
❖ Very mild hyperbola: 3.1 μm departure

Non-null measurement
(spherical reference)

(this asphere is close to the slope limit of a standard interferometer)



Deviation from asphere
(nominal prescription subtracted from the measurement)



Non-null test issues

❖ Fringe resolution

- ❖ **Dense fringes cannot be resolved, limiting the amount of aspheric departure measurable in a non-null test**

❖ Retrace error

- ❖ **Many fringes in view cause a loss of accuracy that depends on the local fringe density**

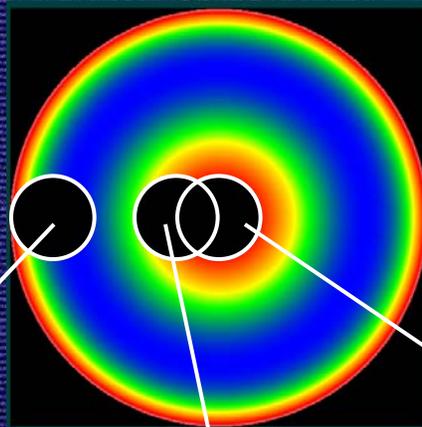
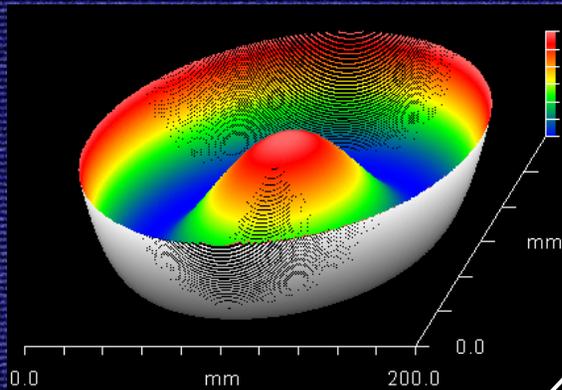
❖ Alignment

- ❖ **More sensitive to lateral calibration and distortion**
- ❖ **Tilt and translation are not equivalent (e.g. induced coma)**
- ❖ **Confocal position is ill-defined (continuum of pseudo-nulls)**

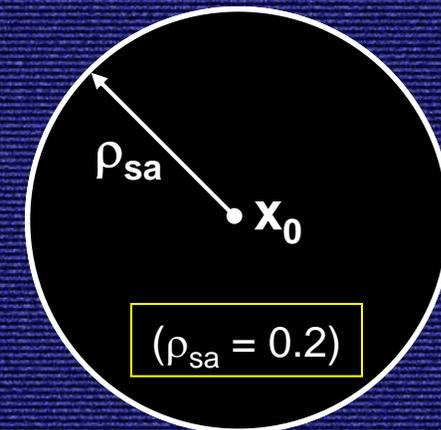
❖ *QED is developing software to alleviate these issues*

Extended longitudinal range example

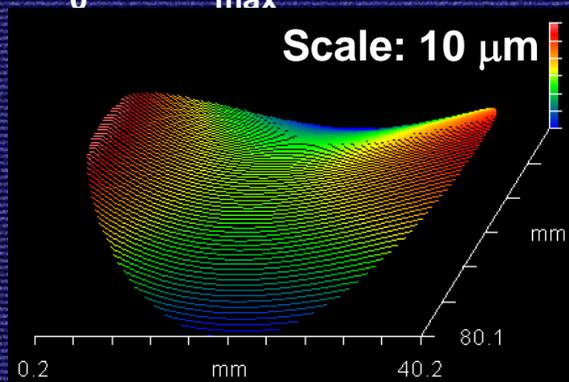
4th order sag, scale: PV 25 μm



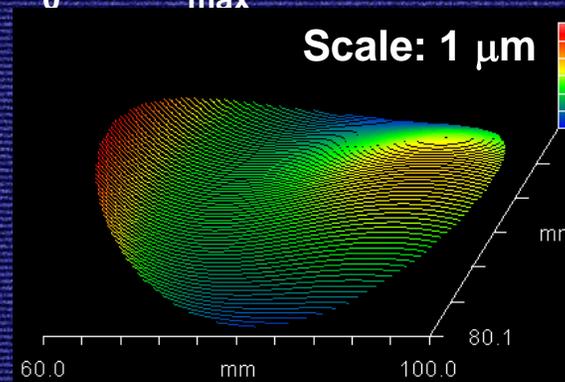
Subaperture close up



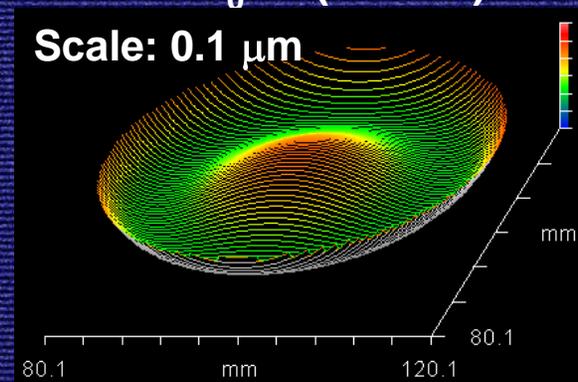
$x_0: 0.8 r_{\text{max}}$



$x_0: 0.2 r_{\text{max}}$



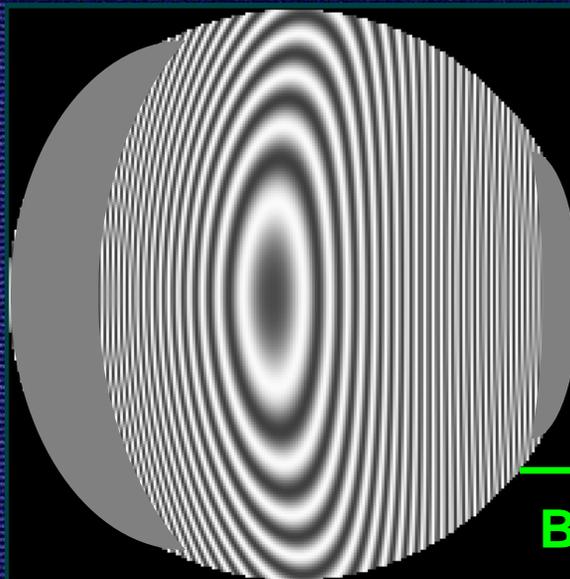
$x_0: 0$ (center)



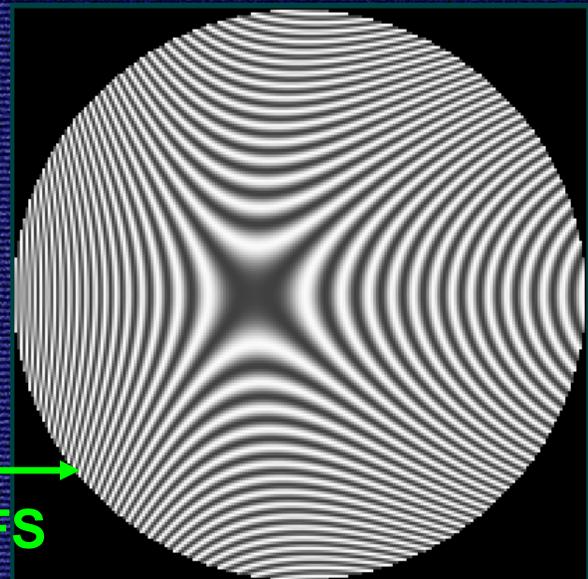
Vertical range extension

- ❖ From 25 to 10 μm may not seem like much, but...
 - ❖ measurement limits are usually driven by *slope*
 - ❖ spherical slope is $\sim 10\times$ astigmatism for a given PV
 - ❖ XF of 5 can get a vertical dynamic range extension of up to 25x

80% zone subaperture



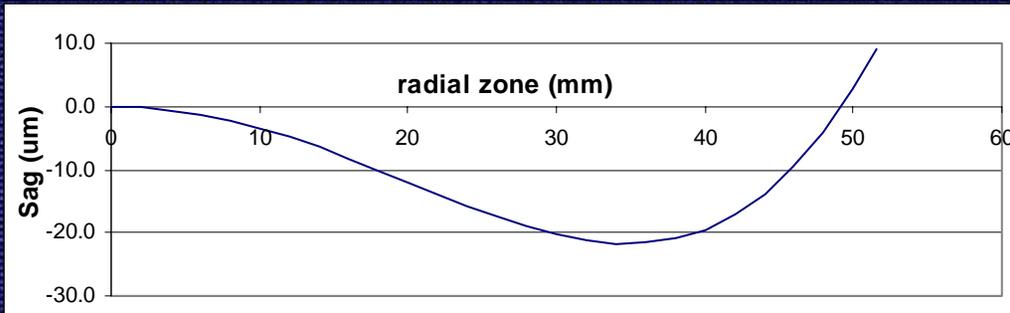
10 μm astigmatism



BFS

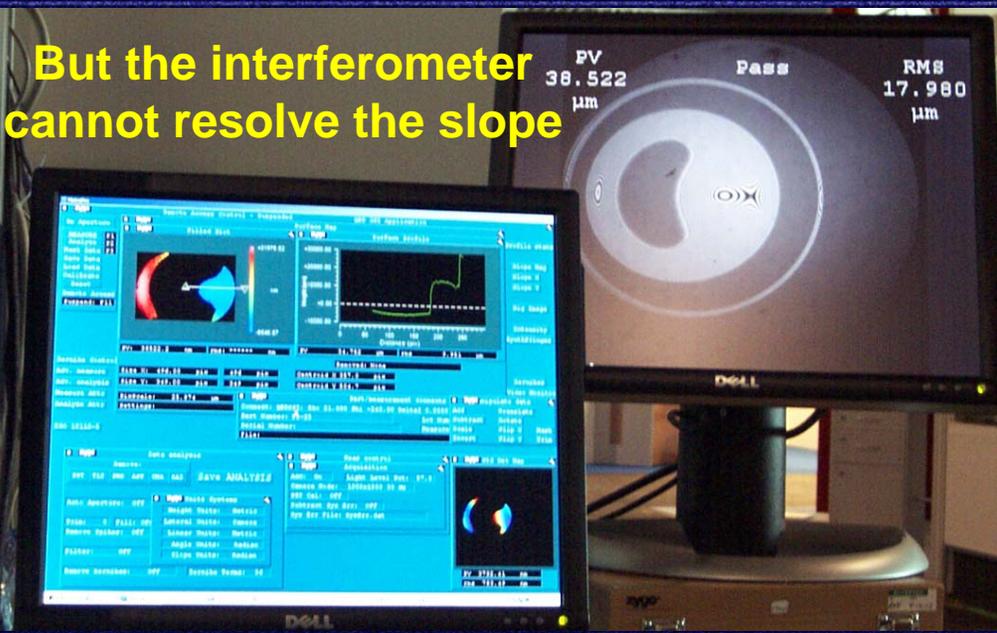
Example asphere measurement

❖ Live at Optatec show, June 2004



But the interferometer cannot resolve the slope

PV 38.522 μm Pass RMS 17.980 μm



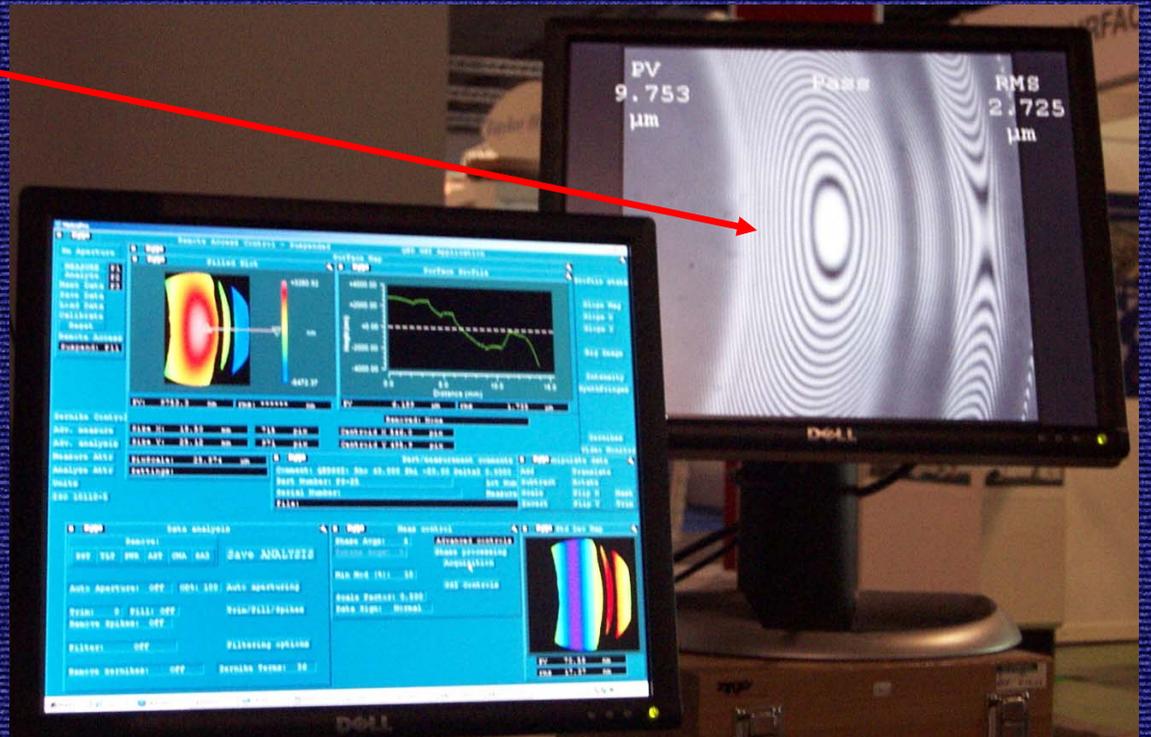
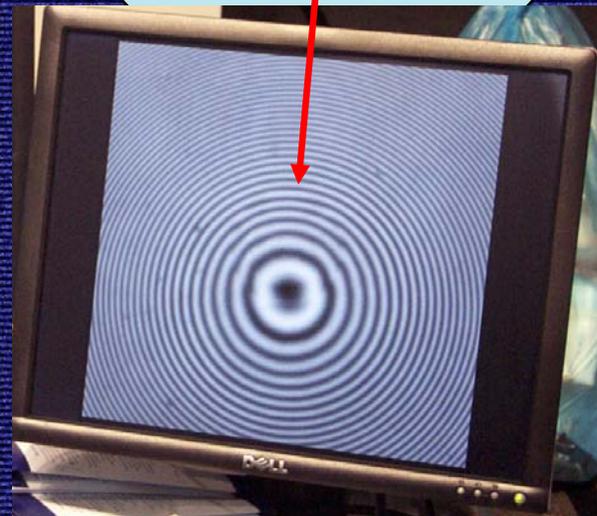
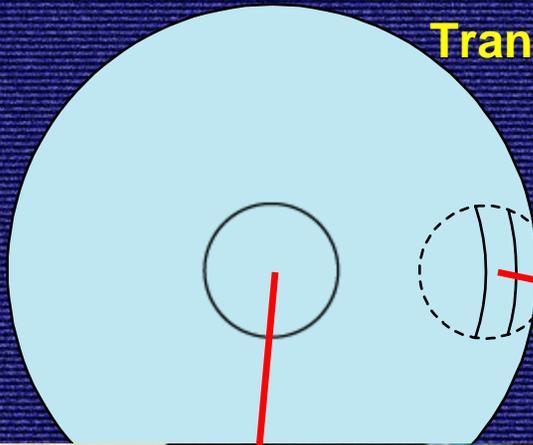
Part OD only 115 mm (< 6" transmission flat)

Acquisition in progress

❖ Measurement time ~30 min (~70 subapertures)

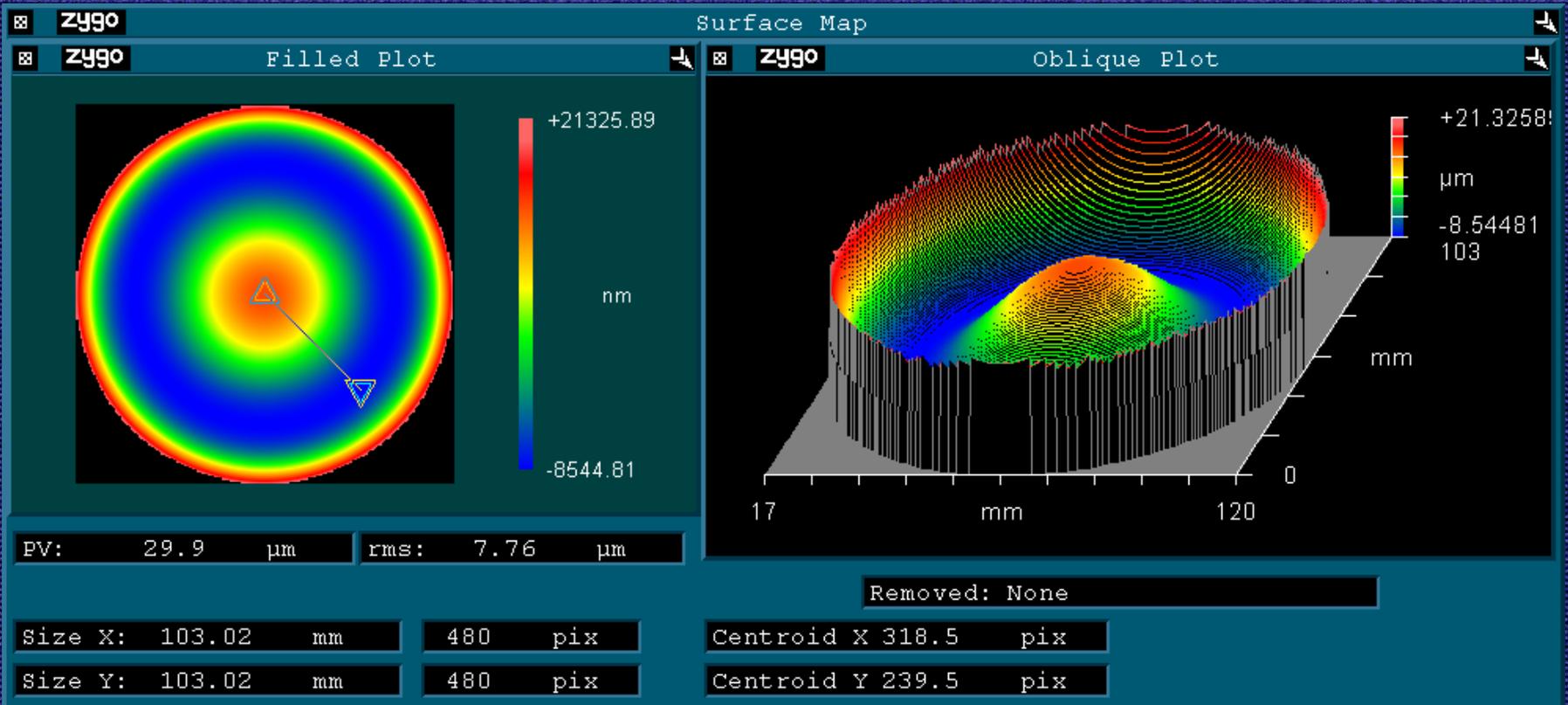
Transmission flat used at 6x zoom (~25 mm field of view)

Outer subapertures are < 25 mm
(data dropout at the edges)



Stitching results

- ❖ Deviation of the part from a plane
 - ❖ accuracy analysis pending



Asphere roadmap

- ❖ Presently: up to $\sim 3 \mu\text{m}$ (w/o SSI), $\sim 10 \mu\text{m}$ (w/ SSI)
 - ❖ User skill is required to address shape subtraction, alignment compensation, and retrace error assessment

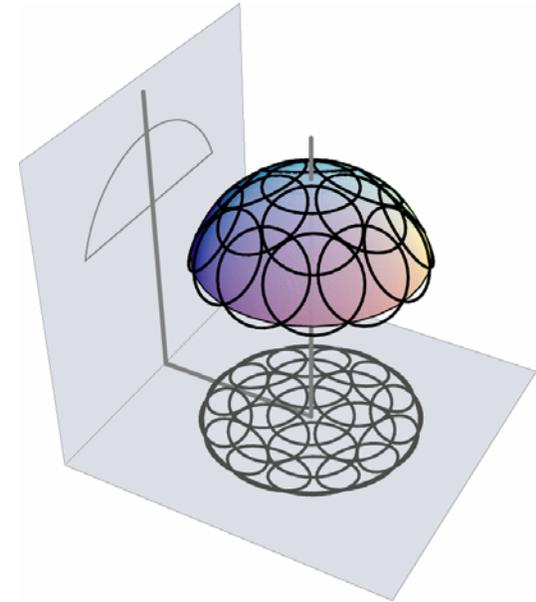
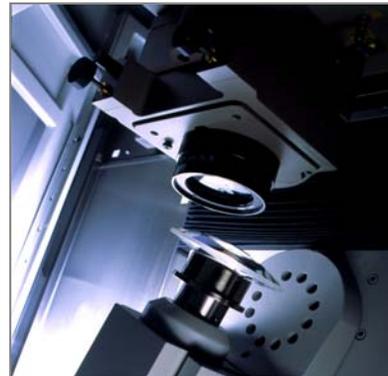
- ❖ Mild asphere software for SSI
 - ❖ Current capability (ready to test)
 - ❖ Acquire data on aspheres with $\sim 30\text{-}50\text{+?} \mu\text{m}$ of departure
 - ❖ Subtraction of aspheric shape from non-null test
 - ❖ Under development
 - ❖ Automatic lattice design
 - ❖ Improved error compensation

- ❖ Moderate departure asphere system
 - ❖ In R & D

Comments on first asphere test

- ❖ This first attempt demonstrates promising results
- ❖ But many unanswered *scientific* questions remain!
 - ❖ Complete characterization of performance
 - ❖ Uncertainty in the null measurement
 - ❖ Repeatability / reproducibility of stitched measurement
 - ❖ How fast does the accuracy degrade with slope?
 - ❖ What is the sensitivity to poor part figure?
 - ❖ What performance improvements are reasonable?
 - ❖ Lattice optimization
 - ❖ Retrace calibration
 - ❖ Other data pre-processing / inteferometer setting management
 - ❖ Etc.

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